

REPORT OF PRELIMINARY SUBSURFACE INVESTIGATION AND GEOTECHNICAL EVALUATION

PROPOSED WIND TURBINES ROARING BROOK WIND POWER PROJECT TOWN OF MARTINSBURG LEWIS COUNTY, NEW YORK

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ATL Report No. WTCD2907E-01-08-08

September 29, 2008

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PRELIMINARY SUBSURFACE INVESTIGATION AND GEOTECHNICAL EVALUATION

PROPOSED WIND TURBINES AND SUBSTATIONS ROARING BROOK WIND POWER PROJECT TOWN OF MARTINSBURG LEWIS COUNTY, NEW YORK

ATL ENGINEERING, P.C.

1.0 INTRODUCTION

At the request of Mr. Donald F. Hammond, representing Iberdrola Renewables, Atlantic Testing Laboratories, Limited (ATL) performed a preliminary subsurface investigation and geotechnical evaluation for the referenced project to ascertain the general subsurface soil and groundwater conditions at select wind turbine locations and two substation locations. The purpose was to evaluate the engineering significance of these findings, and to provide preliminary recommendations related to foundation design and construction. The subsurface investigation was performed on August 26 and 27, 2008.

The project consists of constructing thirty-nine (39) wind turbines, two (2) substations, and associated underground and overhead interconnect lines in the Town of Martinsburg located in Lewis County, New York. The project coordinates at the approximate center of the site are N 43° 42' 51" latitude and W 75° 36' 34" longitude. A **Site Location Plan** is included in **Appendix A**.

The preliminary subsurface investigation consisted of the excavation of shallow test pits at seven (WTG-2, WTG-10, WTG-12, WTG-18, WTG-21, WTG-29, WTG-33) of the proposed thirty-nine turbine locations, one (TP-33/34) along the proposed buried transmission route, and three test pits at the proposed substations. The test pit locations were selected by ATL and approved by Iberdrola Renewables, formerly PPM Energy, Inc., to provide spatial coverage across the proposed project area.

All elevations and dimensions referenced in this document are reported in units of feet, unless otherwise indicated.

2.0 PROJECT DESCRIPTION

The following information, regarding the proposed wind turbine generators, was provided to ATL by Iberdrola Renewables. The proposed wind turbines will be Gamesa 2.0 MW G90 wind turbines. The turbines will be supported on towers approximately 100 meters (328 feet) high at the rotor hub with a rotor diameter of approximately 90 meters (295 feet).

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The anticipated turbine foundations consist of a shallow concrete spread footing founded at a depth of approximately 10 feet below grade, and approximately 50 to 60 feet in diameter.

Information regarding the substation foundation details and loading were not provided at the time of report issuance.

3.0 PREVIOUS INVESTIGATION

A Desktop Study was previously performed by ATL, AE Report No. AE031-01-09-07, dated September 27, 2007, in support of the project. The desktop study indicated that it may be feasible to support the wind turbines on a shallow foundation system bearing on suitable in-situ soil, or compacted engineered fill, or stone columns. Potential geotechnical and geologic risks identified in the study were flooding/high ground water due to wetlands and low permeable site soils, caves/karst due to underlying limestone bedrock, swelling/shrinking clay soil and corrosive soils.

Previous subsurface investigation and geotechnical evaluations were performed by ATL at the 195 turbine Maple Ridge wind project located approximately 1 to 2 miles northeast of the proposed Roaring Brook project site.

4.0 GENERAL SITE CONDITIONS AND GEOLOGY

The proposed project site generally consists of forested rolling hills and agricultural fields. There are interconnected gravel roads within the project area, which were previously constructed by the land owner.

The proposed Roaring Brook wind project is located approximately 7 miles west of Lowville, on the Tug Hill Plateau. The Tug Hill Plateau is located to the west of the Adirondack Mountains, separated by the Black River valley, and to the east of the Ontario Lowlands. Due to the rural, forested nature of the proposed site, the NRCS has not conducted a detailed soil survey of the entire project area.

Based on the Surficial Geologic Map of New York, Adirondack Sheet, the site is generally covered with glacial till that is overlain by lacustrine silty sand. The glacial till varies in texture from boulders to silt, with poorly sorted sand-rich material exhibiting variable permeability. The thickness of the glacial till can range from 3 to 165 feet (1 to 50 meters). Swamp deposits, till moraine, and exposed rock also exist in the project area. The swamp deposits consist of peat-muck, organic silt and sand in poorly drained areas. The thickness of the swamp deposits can range between 3 to 33 feet (1 to 10 meters). Areas to the east and west contain till moraine. Till moraine is variable in size and sorting, with minor amounts of sand and silt that was deposited during the final melting of the glaciers. The thickness of the till moraine ranges from 3 to 33 feet (1 to 10 meters).

Based on the Geologic Map of New York, Adirondack Sheet, the underlying bedrock profile consists of siltstone and shale of the Pulaski and Whetstone Gulf formations underlain by Utica shale. The siltstone and shale are underlain by bedrock formations of the Trenton and Black River Groups, which may consist of limestone, shale, and siltstone. At the southern end of the project site, a cap of Oswego sandstone may exist over the Pulaski and Whetstone formation. The bedrock is primarily marine sediment of

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early to mid-Ordovician age (about 400 million years old). The bedrock is relatively flatlying and undeformed. Within the last 12,000 to 1 million years, the area was covered by glaciers which removed material and rounded the topography, leaving behind glacial till (unsorted clay-rich soil) and outwash (sand and gravel). The geologic conditions mapped at the Roaring Brook site appear similar to the conditions mapped at the Maple Ridge site.

Based on a review of the Maple Ridge Phase 1 subsurface investigation and geotechnical evaluation report (ATL Report No. CD2398E-2-06-05, dated June 10, 2005), the soil conditions at the Maple Ridge Project consisted of loose sand to very compact glacial till, underlain by weathered rock at depths ranging from 2.0 to 30.5 feet below the surface. Competent limestone, shale and siltstone were reportedly encountered at depths ranging from 4.0 to 35.4 feet below the surface. Based on groundwater measurements and soil moisture content, the groundwater table was encountered at depths ranging from 0.5 to 27 feet below the surface. The report indicates that some of the water encountered may be a perched water condition due to the relative impervious nature of the very compact glacial till and underlying bedrock.

5.0 SUBSURFACE INVESTIGATION & SAMPLING METHODOLOGY

Test pits were advanced within the foundation footprint of the proposed wind turbine and substation locations. The tower and substation centers were staked in the field and the surface elevations were obtained by Thew Associates PE/LS, PLLC. Where test pits could not be performed at the staked location due to access limitations, the test pits were offset. The approximate test pit offsets are provided on the test pit logs. A **Turbine Site Plan, Substation Preliminary Grading Plan, and the staked location coordinates** are included in **Appendix B**.

The test pits were excavated using a Kamatsu WB140 rubber tired backhoe at select turbine locations to evaluate the soil and groundwater conditions, and to collect bulk soil samples for laboratory testing. The soil samples were visually classified in the field by a geotechnical engineer using the Burmister Soil Classification System. The **Test Pit Logs** and **Select Photographs** are included in **Appendix C and D**, respectively.

The test pits were backfilled with on-site soil upon completion. It is important that the backfilled test pits be monitored for settlement or subsidence. This will be the responsibility of Iberdrola Renewables. ATL assumes no liability for test pit settlement.

6.0 SITE SUBSURFACE CONDITIONS

The following description of subsurface conditions is based on the soil and groundwater encountered at the locations investigated. Actual subsurface conditions may vary in both the horizontal and vertical dimensions. Detailed subsurface descriptions are provided on the individual Test Pit Logs.

6.1 Test Pits

6.1.1 Wind Turbine Locations

The wind turbine test pits generally encountered a surficial 10 to 12 inch layer of topsoil and forest cover underlain by silt and sand with varying portions of gravel and cobbles

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that extended to depths ranging from 1.8 to 3 feet below the surface. Underlying the silt and sand was sand and gravel with varying portions of silt and cobbles that extended to test pit termination at depths ranging from 7.5 to 9 feet below the surface. Due to the very compact nature of the subsurface soils and the presence of cobbles, the test pits were generally terminated due to bucket refusal of the excavation equipment.

6.1.2 Buried Transmission Location

Test pit TP-33/34, performed in the area of the proposed buried transmission line, encountered a surficial 10 to 12 inch layer of topsoil and forest cover underlain by sand with varying portions of gravel, silt, and cobbles that extended to test pit termination due to bucket refusal at a depth of 6 feet below the surface.

6.1.3 Substation Locations

At the west substation location, test pit TP-SS1A encountered a surficial 6-inch layer of topsoil and organic material underlain by clayey silt that extended to a depth of 7 feet below the surface. Underlying the clayey silt was sand with varying portions of gravel, silt, and cobbles that extended to test pit termination at the depth of 9.5 feet. Test pit TP-SS1B encountered a surficial 6-inch layer of topsoil and organic material underlain by clayey silt that extended to a depth of 5 feet below the surface. Underlying the clayey silt was gravel with varying portions of sand and silt that extended to 7 feet. Underlying the gravel was sand with varying portions of gravel, silt, and cobbles that extended to test pit termination at the depth of 7 feet.

At the east substation location, test pit TP-SS2 encountered a surficial 6-inch layer of topsoil and organic material underlain by silty sand that extended to a depth of 2.5 feet below the surface. Underlying the silty sand was sand with varying portions of gravel, silt, and cobbles that extended to test pit termination at the depth of 9.5 feet.

A Test Pit Summary Table is included in Appendix E.

6.2 Groundwater

6.2.1 Wind Turbine Locations

Groundwater was observed in test pits WTG-10, WTG-12, and WTG-18 during the test pit excavations. Slight groundwater seepage was encountered in test pit WTG-10 at depths between 4 and 4.5 feet below the ground surface. Groundwater seepage was encountered in test pit WTG-12 at depths between 6 and 8 feet below the ground surface and in test pit WTG-18 at depths between 7 and 10.5 feet below the ground surface. Sidewall sloughing was observed in test pits WTG-12 and WTG-18 due to the water seepage.

6.2.2 Substation Locations

Slight groundwater seepage was encountered in test pit TP-SS1B at a depth of 7 feet below the ground surface. Groundwater was not observed at the other substation locations.

7.0 ELECTRICAL RESISTIVITY

7.1 Field Ground Resistivity Tests

Electrical resistivity tests were performed utilizing a Nilsson Model 400, Soil Resistivity Meter, Serial No. 4-7542, in accordance with IEEE Std. 81-1983.

Two perpendicular tests were performed at turbine locations WTG-2, WTG-10, WTG-21, and WTG-29 and at the two proposed interconnect substations. The tests were performed using spacings of 5, 10, 15, and 20 feet. The values for each of these tests are shown in the **Soil Resistivity Test Field Reports** included in **Appendix F**.

8.0 LABORATORY ANALYSES

Select soil samples were submitted to ATL's geotechnical laboratory for analyses. The laboratory tests included Particle Size Analysis, Moisture Content Determination, Laboratory Compaction, Atterberg Limits, Thermal Resistivity, and Chemical Analysis. The samples were selected based on our field observations and the subsurface soil conditions encountered in the test pits.

8.1 Particle Size Analysis

Six (6) soil samples were selected for particle size analysis at turbine locations WTG-2, WTG-10, WTG-18, TP-33/34, and at substation locations TP-SS1A and TP-SS2. The tests were performed in accordance with ASTM D422 "Particle Size Analysis of Soils." The test results are summarized in the **Particle Size Analysis Summary Table** provided in **Appendix G**.

Soil samples collected from test pit excavations are generally classified using the Unified Soil Classification System (USCS), with group symbols GM for WTG-2, SM for WTG-10, WTG-18, TP-33/34, and TP-SS2 and CL for TP-SS1A.

8.2 Moisture Content

Twelve (12) soil samples were selected for natural moisture content determination. The tests were performed in accordance with ASTM D2216 "Laboratory Determination of Water (Moisture) Content of Soil and Rock." The test results are located on the test pit logs.

The natural moisture content of the samples collected at the turbine locations ranged between 8.7 and 14.6 %. The natural moisture content of the samples collected at the substation locations ranged between 9.9 and 33.4 %.

8.3 Atterberg Limits

Five (5) soil samples were selected for Atterberg Limits determination at locations WTG-2, WTG-10, WTG-18, and TP-33/34 and at substation location TP-SS1A. The tests were performed in accordance with ASTM D4318 "Liquid Limit, Plastic Limit, and Plasticity Index of Soils." The test results are summarized in the **Atterberg Limits Results Table** provided in **Appendix H**.

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The plasticity index of the samples analyzed were classified as non-plastic for WTG-2, WTG-10, WTG-18, and TP-33/34. The clayey silt sample analyzed for TP-SS1A had a plasticity index of 8.

8.4 Laboratory Compaction

Five (6) soil samples were selected for Laboratory Compaction testing at locations WTG-10, WTG-18, TP-33/34, WTG-2 and at substation locations TP-SS1A, and TP-SS2. The tests were performed in accordance with ASTM D1557 "Laboratory Compaction Characteristics of Soil Using Modified Effort." The test results are summarized in the **Laboratory Compaction Results Table** provided in **Appendix I**.

The corrected optimum moisture content and corrected maximum dry density of the sand and gravel samples collected ranged between 5.3 and 6.4 %, and 132.0 and 139.2 pcf, respectively, with the exception of the silty sand sample collected at substation location TP-SS1A. The optimum moisture content and corrected maximum dry density of the silty sand was 12.8 % and 117.4 pcf, respectively.

8.5 Chemical Analysis

Three (3) soil samples were selected for pH, chlorides, and soluble sulfate determination at locations WTG-10, WTG-18, and TP-33/34. The test results are summarized in the **Table of Chemical Analysis** provided in **Appendix J**.

The pH of the samples analyzed ranged between 6.0 and 6.3 standard units (S.U.). The chloride results in all the samples analyzed were less than 0.10 %, and the soluble sulfate results ranged were less than 0.10 %.

8.6 Thermal Resistivity

Three (3) soil samples were selected for thermal resistivity analysis at natural and dry moisture conditions at turbine locations WTG-10, WTG-18, and buried transmission line location TP-33/34. The test results are summarized in the **Table of Thermal Resistivity Analysis** provided in **Appendix K**.

The thermal resistivity of the samples analyzed ranged between 4.231 and 6.953 Mk/w in dry conditions, and between 0.491 and 0.634 Mk/w at natural moisture conditions.

9.0 GEOTECHNICAL ENGINEERING DISCUSSION

9.1 Subsurface Soil Conditions

9.1.1 Wind Turbine Locations

The turbine test pits generally encountered a surficial 10 to 12 inch layer of topsoil and forest cover underlain by silt and sand with varying portions of gravel and cobbles that extended to depths ranging from 1.8 to 3 feet below the surface. The silt and sand was underlain by sand and gravel that extended to test pit termination depths ranging from 7.5 to 9 feet. Based on our observations, the consistency of the sand and gravel appears to range from medium compact to very compact. Cobbles and boulders were

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observed throughout the depths of the test pit excavations and at the surface across the project area.

Weathered rock or bedrock was not encountered within the test pit excavations and visible areas of exposed bedrock were not noted around the test pit areas. Since bedrock was not encountered during the test pit excavations, an evaluation of the potential for karst formations could not be made during this investigation. A site walkover at the time of the test pit excavations did not reveal the presence of any visual sinkholes or other surface depressions that may be indicative of underlying karst formations. Based on our experience at the Maple Ridge project, karst formations were not encountered during the site investigations or during construction. Further evaluation of the potential for karst formations to exist within the project area should consist of supplemental soil borings to evaluate the type, depth, and condition of the underlying bedrock. If warranted, further analysis using geophysical techniques could be performed.

Soils subject to swelling or shrinking were not encountered in the test pits.

The natural moisture content of the soils encountered is generally greater than the optimum moisture content determined from the laboratory compaction tests. Based on the test results and our experience with these soil types, significant moisture conditioning of the on-site soil is not anticipated for use as foundation backfill.

The percentage of fines passing the No. 200 sieve contained in the samples ranged between 21 and 26%. Based on the fines content, the site soils are considered moisture sensitive and frost susceptible, and may become unstable when exposed to repetitive construction traffic and excessive moisture.

9.1.2 Substation Locations

The substation test pits generally encountered a surficial 6-inch layer of topsoil underlain by clayey silt with varying portions of sand, and gravel that extended to depths ranging from 0.5 to 7 feet below the surface. The clayey silt was underlain by sand with varying portions of silt, and gravel that extended to test pit termination depths ranging from 8 to 9.5 feet.

Soils subject to swelling or shrinking were not encountered in the test pits.

The natural moisture content of the clayey silt soils encountered at the substation location is generally greater than the optimum moisture content determined from the laboratory compaction tests. Based on the test results and our experience with these soil types, the clayey silt is generally considered unsuitable for use as fill within the substation footprint.

The percentage of fines passing the No. 200 sieve contained in the clayey silt was 83%. Based on the fines content, the site soils are considered moisture sensitive and frost susceptible, and will become unstable when exposed to repetitive construction traffic.

9.2 Groundwater Conditions

9.2.1 Wind Turbine Locations

Based on test pit observations, groundwater seepage was observed at turbine test pit locations WTG-10, WTG-12, and WTG-18. Slight groundwater seepage was observed at WTG-10 at a depth of 4 feet. Groundwater seepage observed at locations WTG-12 and WTG-18, at depths ranging from 6 to 7 feet, resulted in sidewall sloughing. Based on our knowledge of the project area, a perched groundwater condition may exist during the wetter periods of the year. Supplemental investigation activities consisting of soil borings and rock coring at each of the turbine locations along with the installation of monitoring wells is required to determine the actual groundwater conditions for final foundation design. It is recommended that groundwater monitoring be performed through the end of the spring season, which typically exhibits high precipitation levels, and runoff from snowmelt.

Fluctuations in groundwater levels may occur due to seasonal and climatic variations, changes in the surface runoff patterns, construction activity, and subsequent site development, along with other interrelated factors.

Based on the observed groundwater conditions and our experience at the Maple Ridge project, it is anticipated that the majority of groundwater encountered during foundation excavations should be controlled by pumping from trenches or sumps installed around the perimeter of the foundation excavations.

9.2.2 Substation Locations

Based on test pit observations, slight groundwater seepage was observed at the west substation location TP-SS1B at the depth of 7 feet below the surface. Groundwater was not observed at the other substation test pit locations.

9.3 Shallow Foundations

Based on the information collected during the preliminary subsurface investigation, the subsurface conditions appear suitable for support of the turbine and substation foundations on shallow foundation systems. To provide adequate frost protection, shallow foundations should be founded a minimum of 5 feet below final exterior grade. Excavations for foundations may encounter cobbles, boulders, weathered bedrock, sound bedrock, and ground or surface water during the wetter periods of the year.

Supplemental subsurface investigation activities consisting of soil borings and rock coring at each of the proposed turbine and substation locations, seismic testing, and additional laboratory testing of recovered soil and rock samples is required to evaluate soil and rock parameters, and groundwater conditions for final foundation design.

9.3.1 Wind Turbines

Typical octagonal spread foundation designs have foundation diameters ranging from 50 to 60 feet and are usually founded at depths up to 10 feet below finished grade. Based on our observations and experience with the sand and gravel soils encountered in the

test pits, a safe allowable soil bearing pressure of 4000 pounds per square foot (psf) may be utilized for preliminary foundation design. Supplemental soil borings with Standard Penetration Tests (SPT) are required at each proposed turbine location to evaluate the safe allowable soil bearing capacity for final foundation design.

At turbine locations where the excavation is advanced below groundwater and/or the bearing subgrade is wet or saturated, the subgrade should be overexcavated 6-inches and a 6-inch layer of NYSDOT Number 2, crushed stone placed in the bottom of the excavation to provide a dewatering media and to stabilize the bottom of the excavation. The number 2, crushed stone should be compacted with four passes of a walk behind, dual drum, vibratory roller or diesel plate tamper (Wacker DPU6055 or equivalent) under the direction of a geotechnical engineer. The foundation can then be supported on the number 2, crushed stone. The number 2, crushed stone should be placed and compacted as soon as possible after the excavation is complete.

Based on our experience at the Maple Ridge project, loose or unstable soil conditions may exist within a few feet below the planned bottom of footing depths at some proposed turbine locations. The results of supplemental soil borings should identify the location and estimated depths of the loose soil conditions. Where shallow, loose or unstable soil conditions are encountered, overexcavation and replacement with compacted structural fill may be required to support the foundations. All structural fill should be compacted to densities in excess of 95% of the maximum dry density as determined by ASTM D1557, or as directed by a geotechnical engineer.

9.3.2 Substations

Based on the existing and proposed site contours depicted on the preliminary grading plan prepared for the substation locations, an approximate 2-foot cut and fill is estimated to achieve the finished grade at substation location 1. At substation location 2, an approximate 5-foot cut and 3-foot fill are estimated. Footings founded at a depth of 5 feet will likely bear on a combination of clayey silt and silty sand at the substation locations.

Based on our test pit observations, a safe allowable soil bearing pressure ranging between 1000 and 2000 psf may be utilized for preliminary substation foundation design. Due to the high fines content and moisture condition of the clayey silt, imported fill should be utilized to raise the site grades within the substation footprints. Supplemental soil borings with Standard Penetration Tests (SPT) are required to evaluate the safe allowable soil bearing capacity for final foundation design. At a minimum, soil borings should be performed at the four corners and center of each of the proposed substation locations.

9.4 Foundation Stiffness

Seismic testing consisting of MASW and seismic refraction should be performed at select turbine locations to evaluate poisson's ratio, shear modulus, and quality of the underlying soil and bedrock at the project site.

9.5 Sliding Stability

A coefficient of friction value of 0.45 may be used for preliminary foundation design to evaluate sliding stability of the turbine foundations for concrete footings founded on the in-situ sand and gravel soils. Substation footings founded on the silt soils may be designed using a coefficient of friction value of 0.30.

9.6 Turbine Foundation Backfill

The on-site soils at the turbine locations appear suitable for use as foundation backfill, provided the compacted backfill provides sufficient weight for overturning stability. All turbine foundation backfill should have a maximum particle size limited to 6 inches, or less, and should be compacted to the minimum required unit weight specified by the structural engineer and a minimum of 90% of the maximum dry density, as determined by ASTM D 1557. The sites must be graded to convey water away from the tower foundations.

9.7 Chemical Analysis

Based on a chemical analysis of select soil samples, the soils encountered at the test pit locations ranged from slightly acidic to neutral and sulfate exposure from the foundation soil is considered negligible. A Type I or II cement may be utilized for foundation concrete.

10.0 SUMMARY

The test pit logs and this report in its entirety are presented as a preliminary subsurface investigation and geotechnical evaluation, and may not be representative of the site subsurface conditions across the entire project area, but only what was found at the individual test locations at the time the preliminary investigation was performed. The subsurface soil and groundwater conditions may be different from those described in this report and on the test pit logs.

This report was prepared to present the findings of our preliminary subsurface investigation and engineering evaluation. Further investigation activities will be required for final foundation design.

Prepared by:

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RMM/BTB/rmm

Reviewed by:

Brian T. Barnes, P.E. Senior Engineer

APPENDIX A

SITE LOCATION PLAN

DELORME

Topo USA® 5.0



APPENDIX B

TURBINE SITE AND SUBSTATION PRELIMINARY GRADING PLAN





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Staked Test Pit Locations and Elevations Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| Staked Test Pit | | | |
|-----------------|--------------|--------------|-----------|
| ID | Northing | Easting | Elevation |
| WTG-2 | 1,361,500.10 | 1,072,421.12 | 1,981.42 |
| WTG-10 | 1,355,421.03 | 1,080,457.06 | 1,925.05 |
| WTG-12 | 1,357,231.23 | 1,071,643.81 | 1,945.19 |
| WTG-18 | 1,351,161.42 | 1,079,113.69 | 1,942.55 |
| WTG-21 | 1,349,841.89 | 1,082,394.93 | 1,950.98 |
| WTG-29 | 1,347,693.36 | 1,073,453.74 | 1,941.88 |
| WTG-33 | 1,345,563.36 | 1,077,180.84 | 1,932.40 |
| SS-1 | 1,358,006.04 | 1,118,258.98 | 1,142.35 |
| SS-2 | 1,358,118.14 | 1,118,673.76 | 1,148.01 |

Coordinates shown hereon reference the North American Datum of 1983, 2007 adjustment (NAD83/07) and are projected on the New York State Plane Coordinate System (Central Zone).

Elevations shown hereon reference the North American Vertical Datum of 1988 (NAVD88).

APPENDIX C

TEST PIT LOGS



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|---|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-2 | |
| Test Pit Location: | _30 Feet South of Proposed Tower Center | Date: | 8/27/08 | |
| | | Elevation: | 1981± | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|----------|------------|---------------|-----------------|
| 8/27/08 | 10:10 AM | 9.0' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Sample Depth of Sample Sample To | | Depth of Change | Classification of Materials ('c' coarse, 'm' medium, 'f' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) |
|------------------|-------------------------------------|------|--------------------|---|
| | | | 1.0 | 12" TOPSOIL and ORGANIC MATERIAL |
| | | | 2.5 | Brown SILT; trace f SAND; some GRAVEL (moist, plastic) |
| 1 | 8.0' | 9.0' | | Brown cmf GRAVEL; some cmf SAND; some SILT (moist, non- plastic) w=9.8% - soil matrix contained approximately 30-40% FLAT COBBLES and BOULDERS up to 30 inches |
| | | | | Test pit terminated at 9.0 feet due to bucket refusal. |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Very hard digging at 8.0 feet
- 3. Rolling Terrain



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|----------------------------------|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-10 | |
| Test Pit Location: | Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1925+ | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|----------|------------|-------------|-----------------|
| 8/26/08 | 11:45 AM | 9.0' | See Note 2 | |
| | | | | |

SOIL STRATIGRAPHY

| | Dept | h of | | CLASSIFICATION OF MATERIALS |
|--------|------|------|----------|---|
| Sample | Sam | ple | Depth of | ('C' COARSE, 'M' MEDIUM, 'F' FINE) |
| Number | From | То | Change | ('AND' 35-50%, 'SOME' 20-35%, 'LITTLE' 10-20%, 'TRACE' 0-10%) |
| | | | 0.8 | 10" TOPSOIL and ORGANIC MATERIAL |
| | | | | Brown SILT; and mf SAND; some cmf GRAVEL (moist, non- |
| | | | | plastic) |
| | | | | soil matrix contained approximately 10% COBBLES |
| | | | 2.5 | |
| 1 | 4.0' | 6.0' | | Brown cmf SAND; and cmf GRAVEL; little SILT (moist, non- |
| | | | | coil matrix contained approximately 20, 40% |
| | | | | - Soli matrix contained approximately 30-40% |
| | | | | COBBLES and BOULDERS up to To Inches |
| | | | | - Large boulder encountered at 7.0 feet |
| | | | | |
| | | | | Test pit terminated at 9.0 feet due to bucket refusal. |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Very slight seepage between 4.0 and 4.5 feet.
- 3. Hard digging at 2.5 feet. Very hard digging at 6.0 feet.

ATL Representative: R. Morrison/B. Barnes



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|----------------------------------|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-12 | |
| Test Pit Location: | Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1945± | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|------|------------|-------------|-----------------|
| 8/26/08 | 6:00 | 9.0' | See Note 2 | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Dept Sam From | h of ple To | Depth of Change | Classification of Materials ('C' Coarse, 'M' medium, 'F' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) | |
|------------------|---------------------|-------------------|--------------------|---|--|
| | | | 1.0 | 12" TOPSOIL and ORGANIC MATERIAL | |
| | | | | Brown SILT; and mf SAND; little cmf GRAVEL (moist, plastic) | |
| | | | 2.0 | | |
| 1 | 7.0' | 8.0' | | Grey cmf SAND; and cmf GRAVEL; trace SILT (wet, non-plastic) w=13.5% soil matrix contained approximately 30-40% COBBLES and BOULDERS up to 24 inches Soil becomes wet at 5.0 feet | |
| | | | | Test pit terminated at 8.0 feet due to sidewall sloughing. | |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Water seepage between 6.0 and 8.0 feet. 3.



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|--|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-18 | |
| Test Pit Location: | 25' Northeast of Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1943+ | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|-------------|-----------------|
| 8/26/08 | 1:10 PM | 10.5' | See Note 2 | |
| 8/26/08 | 1:15 PM | 10.5' | 9.0' | 1934± |

SOIL STRATIGRAPHY

| Sample | Dept Sam | h of ple | Depth of | CLASSIFICATION OF MATERIALS ('C' COARSE, 'M' MEDIUM, 'E' FINE) |
|--------|-------------|-------------|----------|--|
| Number | From | То | Change | ('AND' 35-50%, 'SOME' 20-35%, 'LITTLE' 10-20%, 'TRACE' 0-10%) |
| | | | 0.8 | 10" TOPSOIL and ORGANIC MATERIAL |
| | | | 1.8 | Brown mf SAND; some SILT; and mf GRAVEL (moist, plastic) - soil matrix contained approximately 10% COBBLES |
| 1 | 4.0' | 6.0' | | Brown cmf SAND; some cmf GRAVEL; some SILT (moist, non-plastic) w=11.3% soil matrix contained approximately 20-30% COBBLES and BOULDERS up to 27 inches Soil becomes wet at 6.0 feet |
| | | | | Test pit terminated at 12.5 feet. |

NOTES

1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe

2. Hard digging at 2.5'.

3. Water seepage between 7.0 and 10.5 feet.

ATL Representative: R. Morrison / B. Barnes



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|------------------------------------|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-21 | |
| Test Pit Location: | 30' South of Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1951± | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|---------------|-----------------|
| 8/26/08 | 2:30 PM | 7.5' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample | Dept Sam | h of ple | Depth of | CLASSIFICATION OF MATERIALS ('C' COARSE, 'M' MEDIUM, 'F' FINE) |
|--------|-------------|-------------|----------|---|
| Number | From | То | Change | ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) |
| | | | 1.0 | 12" TOPSOIL and ORGANIC MATERIAL |
| | | | | Brown mf SAND; some cmf GRAVEL; some SILT (moist, plastic) |
| | | | 2.0 | |
| 1 | 7.0' | 8.0' | | Grey mf SAND; some cmf GRAVEL; trace SILT (moist, non- plastic) w=8.8% - soil matrix contained approximately 20-30% COBBLES and BOULDERS up to 30 inches |
| | | | | Test pit terminated at 7.5 feet due to bucket refusal. |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Hard digging at 2.0 feet.

3.

ATL Representative: R. Morrison/B. Barnes



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|----------------------------------|---------------|---------|--|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | WTG-29 | |
| Test Pit Location: | Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1942+ | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|---------------|-----------------|
| 8/26/08 | 4:30 PM | 9.0' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Dept Sam From | h of ple To | Depth of Change | CLASSIFICATION OF MATERIALS ('C' COARSE, 'M' MEDIUM, 'F' FINE) ('AND' 35-50%, 'SOME' 20-35%, 'LITTLE' 10-20%, 'TRACE' 0-10%) | |
|------------------|---------------------|-------------------|--------------------|--|--|
| | | | 1.0 | 12" TOPSOIL and ORGANIC MATERIAL | |
| | | | 3.0 | Brown mf SAND; some GRAVEL; some SILT (moist, non- plastic) | |
| 1 | 8.0' | 9.0' | | Grey mf SAND; some GRAVEL; little SILT (moist, non-plastic) w=14.6% - soil matrix contained approximately 20-30% COBBLES and BOULDERS up to 30 inches | |
| | | | | Test pit terminated at 9.0 feet due to bucket refusal. | |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Very hard digging at 2.0 feet.

3.



| Client: | ATL Engineering, PC | Project No.: | CD2907 | |
|--------------------|----------------------------|---------------|---------|--|
| Project: | Roaring Brook Wind Project | Test Pit No.: | WTG-33 | |
| Test Pit Location: | Proposed Tower Center | Date: | 8/26/08 | |
| | | Elevation: | 1932+ | |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|---------------|-----------------|
| 8/26/08 | 3:15 PM | 7.5' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Dept Sam From | h of ple To | Depth of Change | Classification of Materials ('C' coarse, 'M' medium, 'F' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) | |
|------------------|---------------------|-------------------|--------------------|---|--|
| | | | 0.8 | 10" TOPSOIL and ORGANIC MATERIAL | |
| | | | 2.0 | Brown SILT; trace f SAND; trace GRAVEL (moist, plastic) | |
| 1 | 4.0' | 6.0' | | Grey mf SAND; some cmf GRAVEL; trace SILT (moist, non- plastic) w=8.7% - soil matrix contained approximately 20-30% COBBLES and BOULDERS up to 18 inches | |
| | | | | Test pit terminated at 7.5 feet due to bucket refusal. | |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Very hard digging at 6.0 feet.
- 3. Rolling Terrain



| Client: | ATL Engineering, PC | Project No.: | CD2907 |
|--------------------|--------------------------------------|---------------|----------------|
| Project: | Roaring Brook Wind Project | Test Pit No.: | TP-33/34 |
| Test Pit Location: | South side of Denali Highway between | Date: | 8/26/08 |
| | turbines WTG-33 and WTG-34 | Elevation: | Not Determined |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|---------------|-----------------|
| 8/26/08 | 3:30 PM | 6.0' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Dept Sam From | h of ple To | Depth of Change | Classification of Materials ('c' coarse, 'M' medium, 'f' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) | |
|------------------|---------------------|-------------------|--------------------|--|--|
| | | | 1.0 | 12" TOPSOIL and ORGANIC MATERIAL | |
| | | | | Brown mf SAND; little GRAVEL; some SILT (moist, non-plastic) | |
| | | | 2.5 | | |
| 1 | 4.0' | 6.0' | | Brown cmf SAND; and cmf GRAVEL; some SILT (moist, non- plastic) w=11.5% - soil matrix contained approximately 10-20% COBBLES up to 8 inches | |
| | | | | Test pit terminated at 6.0 feet due to bucket refusal. | |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- Very hard digging at 6.0 feet.
 3.



| Client: | ATL Engineering, PC | Project No.: | CD2907 |
|--------------------|--|---------------|----------------|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | TP-SS1A |
| Test Pit Location: | 40' South of Proposed Center of Substation 1 | Date: | 8/27/08 |
| | | Elevation: | Not Determined |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|----------|------------|---------------|-----------------|
| 8/27/08 | 12:00 PM | 9.5' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample | Dept Sam | h of ple | Depth of | CLASSIFICATION OF MATERIALS ('C' COARSE, 'M' MEDIUM, 'F' FINE) | |
|--------|-------------|-------------|----------|---|--|
| Number | From | То | Change | ('AND' 35-50%, 'SOME' 20-35%, 'LITTLE' 10-20%, 'TRACE' 0-10%) | |
| | | | 0.5 | 6" TOPSOIL and ORGANIC MATERIAL | |
| 1 | 2.0' | 3.0' | | Blue SILT; and CLAY (moist, plastic) | |
| | | | 3.5 | | |
| 2 | 4.0' | 6.0' | | Brown SILT; some CLAY; little mf SAND; trace mf GRAVEL | |
| | | | 7.0 | (wet, plastic) w=33.4% | |
| 3 | 8.0' | 9.0' | | Brown mf SAND; and SILT; some GRAVEL (moist, non-plastic) w=10.5% - soil matrix contained approximately 10-20% COBBLES and BOULDERS up to 8 inches | |
| | | | | Test pit terminated at 9.5 feet due to bucket refusal. | |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Hard digging at 9.0 feet.
- 3. _____



| Client: | ATL Engineering, PC | Project No.: | CD2907 |
|--------------------|--|---------------|----------------|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | TP-SS1B |
| Test Pit Location: | 30' North of Proposed Center of Substation 1 | Date: | 8/27/08 |
| | | Elevation: | Not Determined |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|----------|------------|-------------|-----------------|
| 8/27/08 | 12:30 PM | 9.5' | See Note 2 | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Dept Sam From | Depth of SampleDepth of Depth ofFromToChange | | Classification of Materials ('C' coarse, 'M' medium, 'F' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) |
|------------------|---------------------|--|-----|---|
| | | | 0.5 | 6" TOPSOIL and ORGANIC MATERIAL |
| | | | | Blue SILT; and CLAY (moist, plastic) |
| | | | 5.0 | |
| 1 | 6.0' | 7.0' | | Brown cmf GRAVEL; some cmf SAND; trace SILT (wet, non- |
| | | | 7.0 | plastic) w=16.4% |
| | | | | Brown mf SAND; and SILT; little GRAVEL (moist, non-plastic) - soil matrix contained approximately 10-20% COBBLES up to 8 inches |
| | | | | Test pit terminated at 9.5 feet due to bucket refusal. |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Slight water seepage at 7.0 feet.
- 3. Hard digging at 9.0 feet.



| Client: | ATL Engineering, PC | Project No.: | CD2907 |
|--------------------|----------------------------------|---------------|----------------|
| Project: | Roaring Brook Wind Power Project | Test Pit No.: | TP-SS2 |
| Test Pit Location: | Proposed Center of Substation 2 | Date: | 8/27/08 |
| | | Elevation: | Not Determined |

GROUNDWATER OBSERVATIONS

| Date | Time | Hole Depth | Water Depth | Water Elevation |
|---------|---------|------------|---------------|-----------------|
| 8/27/08 | 1:00 PM | 8.0' | None Observed | |
| | | | | |

SOIL STRATIGRAPHY

| Sample Number | Depth of SampleDepth of Depth of Change | | Depth of Change | Classification of Materials ('C' coarse, 'M' medium, 'f' fine) ('and' 35-50%, 'some' 20-35%, 'little' 10-20%, 'trace' 0-10%) |
|------------------|--|------|--------------------|---|
| | | | 0.5 | 6" TOPSOIL and ORGANIC MATERIAL |
| | | | | Brown SILT; and mf SAND (moist, plastic) |
| | | | 2.5 | |
| 1 | 3.0' | 6.0' | | Brown cmf SAND; some SILT; some cmf GRAVEL (moist, non- plastic) w=9.9% - soil matrix contained approximately 10-20% COBBLES and BOULDERS up to 8 inches |
| | | | | Test pit terminated at 8.0 feet due to bucket refusal. |

NOTES

- 1. Type of Excavator: Komatsu WB140 Rubber Tired Backhoe
- 2. Hard digging at 9.0 feet.
- 3. Test pit located on a slope.

APPENDIX D

SELECT PHOTOGRAPHS

ATLANTIC TESTING LABORATORIES, Limited ATL Report No. WTCD2907E-01-08-08



Photograph 1: View of test pit WTG-10.



Photograph 2: View of test pit WTG-12.

ATLANTIC TESTING LABORATORIES, Limited ATL REPORT NO. CD2907-01-09-08



Photograph 3: View of test pit WTG-18.



Photograph 4: View of test pit WTG-29.

ATLANTIC TESTING LABORATORIES, Limited ATL REPORT NO. CD2907-01-09-08



Photograph 5: View of test pit TP-SS1B



Photograph 6: View of test pit TP-SS2

APPENDIX E

TEST PIT SUMMARY TABLES



ATLANTIC TESTING LABORATORIES

Table 1

Preliminary Subsurface Investigation Summary Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| | Field | Investigation | Laboratory Analysis | | | | | | | |
|-----------------|-------------|---------------------------|---------------------------|---------------------|---------------------|--------------------------|----------------------|------------------------|--|--|
| Test Pit No. | Test Pit | Electrical Resistivity | Particle Size Analysis | Natural Moisture | Atterberg Limits | Laboratory Compaction | Chemical Analysis | Thermal Resistivity | | |
| WTG-2 | 1 | 1 | 1 | 1 | 1 | 1 | | | | |
| WTG-10 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | |
| WTG-12 | 1 | | | 1 | | | | | | |
| WTG-18 | 1 | | 1 | 1 | 1 | 1 | 1 | 1 | | |
| WTG-21 | 1 | 1 | | 1 | | | | | | |
| WTG-29 | 1 | 1 | | 1 | | | | | | |
| WTG-33 | 1 | | | 1 | | | | | | |
| TP-33/34 | 1 | | 1 | 1 | 1 | 1 | 1 | 1 | | |
| TP-SS1A | 1 | 1 | 1 | 1 | 1 | 1 | | | | |
| TP-SS1B | 1 | | | 1 | | | | | | |
| TP-SS2 | 1 | 1 | 1 | 1 | | | | | | |



ATLANTIC TESTING LABORATORIES

Table 2

Test Pit Summary Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| | | Test Pit Data | | | | |
|-----------------|----------|------------------------|------------------------------|--|--|--|
| Test Pit No. | Date | Water Depth (ft) | Termination Depth (ft) | | | |
| WTG-2 | 08/27/08 | None Observed | 9.0 | | | |
| WTG-10 | 08/26/08 | 4.0 | 9.0 | | | |
| WTG-12 | 08/26/08 | 6.0 | 8.0 | | | |
| WTG-18 | 08/26/08 | 7.0 | 10.5 | | | |
| WTG-21 | 08/26/08 | None Observed | 7.5 | | | |
| WTG-29 | 08/26/08 | None Observed | 9.0 | | | |
| WTG-33 | 08/26/08 | None Observed | 7.5 | | | |
| TP-33/34 | 08/26/08 | None Observed | 6.0 | | | |
| TP-SS1A | 08/27/08 | None Observed | 9.5 | | | |
| TP-SS1B | 08/27/08 | 7.0 | 9.5 | | | |
| TP-SS2 | 08/27/08 | None Observed | 8.0 | | | |

Remarks:

Water depths are estimated based on field observations.

APPENDIX F

Soil Resistivity Test Field Reports

ATLANTIC TESTING LABORATORIES, Limited

Soil Resistivity Test Field Report

| JOB NO: | CD2907 |
|---------|-----------|
| DATE: | 19-Sep-08 |

Field Technician:R. MorrisonTest Instrument:Nilsson Model 400Procedure:4 point soil resistivity test

| LOCATION | DEPTH TESTED | METER READING | CALCULATED SOIL RESISTIVITY |
|------------------|-------------------|--|----------------------------------|
| (attach map) | (spacing in feet) | (ohms) | =191.5 x SPACING (ft) x R (ohms) |
| | 5 | 140 | 134,050 |
| WTG_21#1 | 10 | 110 | 210,650 |
| WIG-21 #1 | 15 | 107 | 307,378 |
| | 20 | 92 | 352,360 |
| | 5 | 330 | 315,975 |
| WTG_21#2 | 10 | 170 | 325,550 |
| WIG-21 #2 | 15 | 95 | 272,888 |
| | 20 | METER (ADING CALCOLAT (ohms) =191.5 x S 140 1 110 1 107 92 330 1 92 330 170 95 57 240 120 63 41 250 150 73 48 550 120 94 57 230 150 79 61 250 120 62 51 200 104 41 23 94 | 218,310 |
| | 5 | 240 | 229,800 |
| WTC 20#1 | 10 | 120 | 229,800 |
| VV1G-29#1 | 15 | 63 | 180,968 |
| | 20 | 41 | 157,030 |
| | 5 | 250 | 239,375 |
| WTC 20#2 | 10 | 150 | 287,250 |
| WIG-29#2 | 15 | 73 | 209,693 |
| | 20 | 48 | 183,840 |
| | 5 | 550 | 526,625 |
| WTG 2#1 | 10 | 120 | 229,800 |
| VV 1G-2#1 | 15 | 94 | 270,015 |
| | 20 | 57 | 218,310 |
| | 5 | 230 | 220,225 |
| WTG-2#2 | 10 | 150 | 287,250 |
| WI 0-2#2 | 15 | 79 | 226,928 |
| | 20 | 61 | 233,630 |
| | 5 | 250 | 239,375 |
| WTG_10#1 | 10 | 120 | 229,800 |
| WTG-10#1 | 15 | 62 | 178,095 |
| | 20 | 51 | 195,330 |
| | 5 | 200 | 191,500 |
| WTG-10#2 | 10 | 104 | 199,160 |
| | 15 | 41 | 117,773 |
| | 20 | 23 | 88,090 |

ATLANTIC TESTING LABORATORIES, Limited

Soil Resistivity Test Field Report (con't)

| Test Instrument: | Nilsson Model 400 |
|------------------|-------------------------------|
| Procedure: | 4 point soil resistivity test |

| LOCATION | DEPTH TESTED | METER READING | CALCULATED SOIL RESISTIVITY | | |
|--------------|-------------------|--|----------------------------------|--|--|
| (attach map) | (spacing in feet) | (ohms) | =191.5 x SPACING (ft) x R (ohms) | | |
| | 5 | 8.5 | 8,139 | | |
| TD 991#1 | 10 | TEDMETER READINGCALCULATED S $2et$) $(ohms)$ =191.5 x SPACII 8.5 $8,7$ 5.8 11, 4.8 13, 4.5 17, 5.1 $4,8$ 4.4 $8,4$ 4.4 $8,4$ 4.1 11, 3.7 14, 9.8 $9,5$ 6.3 12, 6.3 12, 6.3 12, 6.3 12, 6.3 15, 4.9 18, | 11,107 | | |
| 17-331#1 | 15 | 4.8 | 13,788 | | |
| | 20 | D METER READING CALCULATED SOl = 191.5 x SPACING 8.5 8,13 5.8 11,10 4.8 13,78 4.5 17,23 5.1 4,88 4.4 8,42 4.1 11,77 3.7 14,17 9.8 9,38 6.3 12,00 6.3 18,09 5.7 21,83 7.5 7,18 6.1 11,68 5.3 15,25 4.9 18,70 | 17,235 | | |
| | 5 | 5.1 | 4,883 | | |
| TD 991#2 | 10 | 4.4 | 8,426 | | |
| 17-331#2 | 15 | 4.1 | 11,777 | | |
| | 20 | 3.7 | 14,171 | | |
| | 5 | 9.8 | 9,384 | | |
| TD 992#1 | 10 | 6.3 | 12,065 | | |
| 17-332#1 | 15 | 6.3 | 18,097 | | |
| | 20 | 5.7 | 21,831 | | |
| | 5 | 7.5 | 7,181 | | |
| TD_997#2 | 10 | 6.1 | 11,682 | | |
| 17-552#2 | 15 | 5.3 | 15,224 | | |
| | 20 | 4.9 | 18,767 | | |

APPENDIX G

PARTICLE SIZE ANALYSIS SUMMARY TABLE



ATLANTIC TESTING LABORATORIES

Table 3

Particle Size Analysis Results Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| Test Pit | Sample | Depth (ft) | Percent Passing | | | | | | | | | | |
|----------|--------|---------------|-----------------|-----|-----|-----|------|------|----|-----|-----|------|---------------|
| No. | No. | | 4″ | 3″ | 2″ | 1″ | 3⁄4‴ | 1⁄2″ | #4 | #10 | #40 | #200 | 0.005 (mm) |
| WTG-2 | S-1 | 8.0-9.0 | 100 | 98 | 84 | 75 | 71 | 66 | 54 | 46 | 36 | 21 | |
| WTG-10 | S-1 | 4.0-6.0 | 100 | 100 | 90 | 84 | 80 | 75 | 64 | 57 | 45 | 26 | |
| WTG-18 | S-1 | 7.0-8.0 | 100 | 100 | 99 | 91 | 87 | 82 | 70 | 59 | 47 | 24 | |
| TP-33/34 | S-1 | 4.0-6.0 | 100 | 100 | 98 | 84 | 81 | 75 | 64 | 59 | 49 | 23 | - |
| TP-SS1A | S-1 | 4.0-6.0 | 100 | 100 | 100 | 100 | 99 | 99 | 97 | 97 | 93 | 83 | 28 |
| TP-SS2 | S-1 | 3.0-6.0 | 100 | 100 | 94 | 90 | 88 | 85 | 78 | 72 | 59 | 32 | |

APPENDIX H

ATTERBERG LIMITS RESULTS TABLE

atl

ATLANTIC TESTING LABORATORIES

Table 4

Atterberg Limits Results Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| Test Pit | Sample | Depth | USCS Soil | Plastic | Liquid | Plasticity |
|----------|--------|---------|----------------|---------|--------|------------|
| No. | No. | (ft) | Classification | Limit | Limit | Index |
| WTG-2 | S-1 | 8.0-9.0 | GM | NP | NP | NP |
| WTG-10 | S-1 | 4.0-6.0 | SM | NP | NP | NP |
| WTG-18 | S-1 | 4.0-6.0 | SM | NP | NP | NP |
| TP-33/34 | S-1 | 4.0-6.0 | SM | NP | NP | NP |
| TP-SS1A | S-1 | 4.0-6.0 | CL | 19 | 27 | 8 |

Remarks:

NP indicates non-plastic.

APPENDIX I

LABORATORY COMPACTION RESULTS TABLE

ATLANTIC TESTING LABORATORIES



Table 5

Laboratory Compaction Results Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| Test Pit No. | Sample No. | Depth (ft) | Natural Moisture Content (%) | Optimum Moisture Content (%) | Maximum Dry Density (pcf) |
|-----------------|---------------|---------------|---------------------------------------|---------------------------------------|---------------------------------|
| WTG-2 | S-1 | 8.0-9.0 | 9.8 | 5.7 | 139.2 |
| WTG-10 | S-1 | 4.0-6.0 | 11.2 | 5.6 | 138.6 |
| WTG-18 | S-1 | 7.0-8.0 | 11.3 | 6.4 | 132.0 |
| TP-33/34 | S-1 | 4.0-6.0 | 11.5 | 5.3 | 138.9 |
| TP-SS1A | S-1 | 4.0-6.0 | 33.4 | 12.8 | 117.4 |
| TP-SS2 | S-1 | 3.0-6.0 | 9.9 | 5.5 | 138.3 |

APPENDIX J

TABLE OF CHEMICAL ANALYSIS



ATLANTIC TESTING LABORATORIES

Table 6

Chemical Analysis Results Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| | | | Chemical Analysis | | | | | | | | | |
|-----------------|---------------|---------------|-------------------|------------------|------------------------|--|--|--|--|--|--|--|
| Test Pit No. | Sample No. | Depth (ft) | рН (S.U.) | Chlorides (%) | Soluble Sulfate (%) | | | | | | | |
| WTG-10 | S-1 | 4.0-6.0 | 6.0 | <0.1 | <0.1 | | | | | | | |
| WTG-18 | S-1 | 4.0-6.0 | 6.3 | <0.1 | <0.1 | | | | | | | |
| TP-33/34 | S-1 | 4.0-6.0 | 6.1 | <0.1 | <0.1 | | | | | | | |

APPENDIX K

TABLE OF THERMAL RESISTIVITY RESULTS

ATLANTIC TESTING LABORATORIES



Table 7

Thermal Resistivity Results Roaring Brook Wind Power Project ATL Report No. CD2907E-01-08-08

| Test Pit | Moisture | Temp | | |
|----------|----------|------|----------------|-------|
| No. | (%) | (C) | R ² | Mk/w |
| WTG-10 | Dry | 25.9 | 1.0000 | 4.231 |
| WTG-10 | 11.2 | 24.2 | 0.9999 | 0.491 |
| WTG-18 | Dry | 26.0 | 0.9999 | 6.953 |
| WTG-18 | 11.3 | 25.3 | 0.9996 | 0.634 |
| TP-33/34 | Dry | 25.5 | 1.0000 | 5.128 |
| TP-33/34 | 11.5 | 24.2 | 0.9994 | 0.503 |

APPENDIX L

LABORATORY TEST REPORTS



Reviewed by: __

Date: <u>9/29/08</u>





Reviewed by: .

Date: 9/29/08





Reviewed by: .

Date: 9/29/08





Reviewed by: _

Date: 9/29/08



Reviewed by:

Date: 9/29/08



Reviewed by: .

Date: 9/26/08



Date: <u>9/29/08</u>



Reviewed by: .

Date: 9/29/08



Reviewed by:

Date: ______08



Environmental LABORATORY SERVICES Certified in: • Connecticut • Massachusetts • New Jersey • New York • Pennsylvania

7280 Caswell Street, Hancock Air Park, North Syracuse, NY 13212 (315) 458-8033, FAX (315) 458-0526, (800) 842-4667

Laboratory Analysis Report

ATLANTIC TESTING LABORATORIES P.O. Box 29 6431 U.S. Highway 11 Canton, NY 13617 ATTN: Mr. Ryan Armstrong

PO#: 70994

PROJECT #: RECEIVED:

230320 09/16/2008 @ 09:30

Site Address: ROARING BROOK WIND FARM

CLIENT JOB NUMBER: CD2907

| TEST PERFORMED |) | RESULTS | UNITS | DATE/TIME PERFORMED | METHOD NUMBER | PERFORMED BY |
|--|--------------------------------|----------------------------------|--|----------------------------------|---|--------------------------------------|
| SAMPLE #: 487072 CHLORIDE SOLIDS, TOTAL SULFATE, SOLUBI | CLIENT SAMPLE ID: LE | T-110, S-1 210 89 720 | MG/KG DRY WT. PERCENT MG/KG DRY WT. | 09/22/08 09/18/08 09/22/08 | DATE/TIME SAMPLED: 03 EPA 325.2 SM18 2540B EPA 375.2 | 8/26/08 @ 13:10 КСН КСН КСН |
| SAMPLE #: 487073 CHLORIDE SOLIDS, TOTAL SULFATE, SOLUBL | ELIENT SAMPLE ID: | T-118, S-1 130 88 800 | MG/KG DRY WT. PERCENT MG/KG DRY WT. | 09/22/08 09/18/08 09/22/08 | DATE/TIME SAMPLED: 08 EPA 325.2 SM18 2540B EPA 375.2 | 3/26/08 @ 13:10 KCH KCH KCH |
| SAMPLE #: 487074 CHLORIDE SOLIDS, TOTAL SULFATE, SOLUBL | CLIENT SAMPLE ID: | T-133/T-134, 150 87 960 | S-1 MG/KG DRY WT. PERCENT MG/KG DRY WT. | 09/22/08 09/18/08 09/22/08 | DATE/TIME SAMPLED: 08 EPA 325.2 SM18 2540B EPA 375.2 | /26/08 @ 15:30 KCH KCH KCH |

ATLANTIC TESTING LABORATORIES P.O. Box 29 6431 U.S. Highway 11 Canton, NY 13617 ATTN: Mr. Ryan Armstrong

PO#: 70994

CLIENT JOB NUMBER: CD2907

TEST PERFORMED

PROJECT #: RECEIVED:

230320 09/16/2008 @ 09:30

ΒY

Site Address: ROARING BROOK WIND FARM

PERFORMED DATE/TIME METHOD PERFORMED NUMBER RESULTS UNITS Sample Receipt Temperature: 19.6Degrees C

Samples received above acceptable temperature requirements of 0-6 degrees C.

1 Lee. David R. Hill

Laboratory Director

09/23/2008 Print Date

All tests performed under NYS ELAP Laboratory Certification # 11375 unless otherwise stated. Report relates only to the samples as received by the laboratory and shall not be reproduced except in full, without written approval from Environmental Laboratory Services.



Page 2 of 2

| Revised: 11/ | OF- |
|--------------|------|
| 1/02 | F-7E |

PO# 70994

Distribution: White with Samples Yellow to Laboratory Pink to ATL Files

— Think Quality –

| Signature: | Name: 5 | Signature: | Name: Roy Composition | Samples Relinquished By: | Sampler's Signature: | Sampler's Name: | | | | | T-133/T-134; S- | T-118; S-1 | T-110; S-1 | Date Time Sample Location | Project Name: Roaring Brook U. | Project Contact: | CD2907 ATL Engineering | Project No. Client Name | Albany Binghamton 22 Corporate Drive 406 North Street 1iffion Park, NY 12065 Endicott, NY 13670 518/383-9144 (T) 607/757-9326 (T) 518/383-9166 (F) 607/757-9252 (F) | |
|---------------|----------|--------------------|----------------------------|--------------------------|----------------------|------------------------|--|--|--|---|-----------------|------------|------------|----------------------------------|--------------------------------|-------------------|------------------------|-------------------------|---|-----------|
| Time: Signat | Date: Na | Time: 16:00 Signat | Date: 9/15/8 Na | | Time: | Date: | | | | | I GS I | C 2 1 | es 1 | Sample No. Type Conta | atem | Project Location | | QA/QC Code | Canton 6431 U.S. Highway 11 Canton, NY 13617 315/386-4578 (T) 316/386-1012 (F) | |
| lure: | Ime: | ure: | ime: | ş | Lab | Re | | | | | ¥ X | X X | × × | iners C | h lo Is l IFe | on brid ble | P 1940 | | Plattsburgh 1080 Military Tumpike Plattsburgh, NY 12901 518/563-5878 (T) 518/562-1321 (F) | DONMENTAL |
| Tir | Da | Tir | Da | amples Received By: | oratory Signature: | eceived for Name: | | | | | | | | | | | | Paramete | Poughkeepsie 251 Upper North Roa Highland, NY 12590 845/691-6098 (T) 845/691-6099 (F) | |
| ne: | tte: | ne: Grab | Ite: Composit | Sampl | 20 the | Anyles | | | | | | | | | | | | SJE | Syracuse 6085 Court Street Road Syracuse, NY 13206 315/699-5281 (T) 315/699-3374 (F) | VIISTODY |
| WW Wastewater | S Soil | GW Groundwater | e <u>DW</u> Drinking Water | e Type Code Key: | Time: 730Av | Date: 2/1/10/03 | | | | - | htotsh | 67073 | eta 8h | Laboratory Identification No. | Fax Results: | | Dates Required: | Report | Utica 301 St. Anthony Street Utica, NY 13501 315/735-3309 (T) 315/735-0742 (F) | 1 NI |
| | | | 19.6.0 | Laboratory Remarks | | Shipment Rec'd Intact? | | | | | | | | Field Notes | ☐ Yes □No tody S | | | Distribution | Watertown P.O. Box 91 Felts Mills, NY 13638 315/773-5390 (T) 315/773-0334 (F) | 2000 |

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